

Natalia Kłosińska

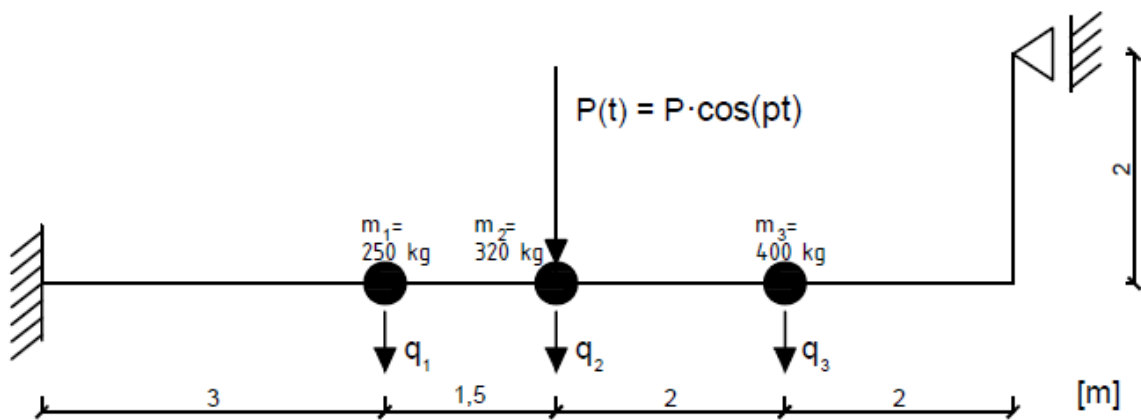
Mechanika budowli

Politechnika Poznańska

Budownictwo 2013/2014

IV semestr, grupa B3

DYNAMIKA – UJĘCIE KLASYCZNE



Dane:

Przekrój: I 220

$I = 3060 \text{ cm}^4$

$W_x = 278 \text{ m}^3$

$E = 205 \text{ GPa}$

$EI = 6273 \text{ kNm}^2 = 6273000 \text{ Nm}^2$

$P = 25,5 \text{ kN} = 25500 \text{ N}$

$p = 10,5 \text{ Hz} = 65,97 \frac{\text{rad}}{\text{s}}$

SSD = 3

1. Wyprowadzenie wzorów do obliczeń:

$$q_i = -A_i \cdot \sin(\omega t)$$

$$\ddot{q}_i = -A_i \cdot \omega^2 \cdot \sin(\omega t)$$

$$\begin{cases} q_1 = \delta_{11}(-m_1\ddot{q}_1) + \delta_{12}(-m_2\ddot{q}_2) + \delta_{13}(-m_3\ddot{q}_3) \\ q_2 = \delta_{21}(-m_1\ddot{q}_1) + \delta_{22}(-m_2\ddot{q}_2) + \delta_{23}(-m_3\ddot{q}_3) \\ q_3 = \delta_{31}(-m_1\ddot{q}_1) + \delta_{32}(-m_2\ddot{q}_2) + \delta_{33}(-m_3\ddot{q}_3) \end{cases}$$

$$\begin{cases} A_1 \cos(\omega t) = \delta_{11}m_1\omega^2 A_1 \cos(\omega t) + \delta_{12}m_2\omega^2 A_2 \cos(\omega t) + \delta_{13}m_3\omega^2 A_3 \cos(\omega t) \\ A_2 \cos(\omega t) = \delta_{21}m_1\omega^2 A_1 \cos(\omega t) + \delta_{22}m_2\omega^2 A_2 \cos(\omega t) + \delta_{23}m_3\omega^2 A_3 \cos(\omega t) \\ A_3 \cos(\omega t) = \delta_{31}m_1\omega^2 A_1 \cos(\omega t) + \delta_{32}m_2\omega^2 A_2 \cos(\omega t) + \delta_{33}m_3\omega^2 A_3 \cos(\omega t) \end{cases}$$

$$\begin{cases} A_1(1 - \delta_{11}m_1\omega^2) - A_2\delta_{12}m_2\omega^2 - A_3\delta_{13}m_3\omega^2 = 0 \\ -A_1\delta_{21}m_1\omega^2 + A_2(1 - \delta_{22}m_2\omega^2) - A_3\delta_{23}m_3\omega^2 = 0 \\ -A_1\delta_{31}m_1\omega^2 - A_2\delta_{32}m_2\omega^2 + A_3(1 - \delta_{33}m_3\omega^2) = 0 \end{cases}$$

2. Obliczenie częstości i postaci drgań własnych:

$$\lambda = \frac{m\omega^2}{EI_0}$$

$$\omega = \sqrt{\frac{\lambda EI_0}{m}}$$

$$m = 100 \text{ kg}$$

$$\delta_{ik} = \sum \int \frac{M_i M_k}{EI} dx$$

$$\delta_{ik} = \frac{1}{EI_0} \delta'_{ik}$$

$$\frac{m_1 \omega^2}{EI_0} = 2,5 \frac{m\omega^2}{EI_0} = 2,5 \lambda$$

$$\frac{m_2 \omega^2}{EI_0} = 3,2 \frac{m\omega^2}{EI_0} = 3,2 \lambda$$

$$\frac{m_3 \omega^2}{EI_0} = 4 \frac{m\omega^2}{EI_0} = 4 \lambda$$

$$\begin{cases} A_1(1 - 2,5\delta'_{11}\lambda) - A_2 3,2\delta'_{12}\lambda - A_3 4\delta'_{13}\lambda = 0 \\ -A_1 2,5\delta'_{21}\lambda + A_2(1 - 3,2\delta'_{22}\lambda) - A_3 4\delta'_{23}\lambda = 0 \\ -A_1 2,5\delta'_{31}\lambda - A_2 3,2\delta'_{32}\lambda + A_3(1 - 4\delta'_{33}\lambda) = 0 \end{cases}$$

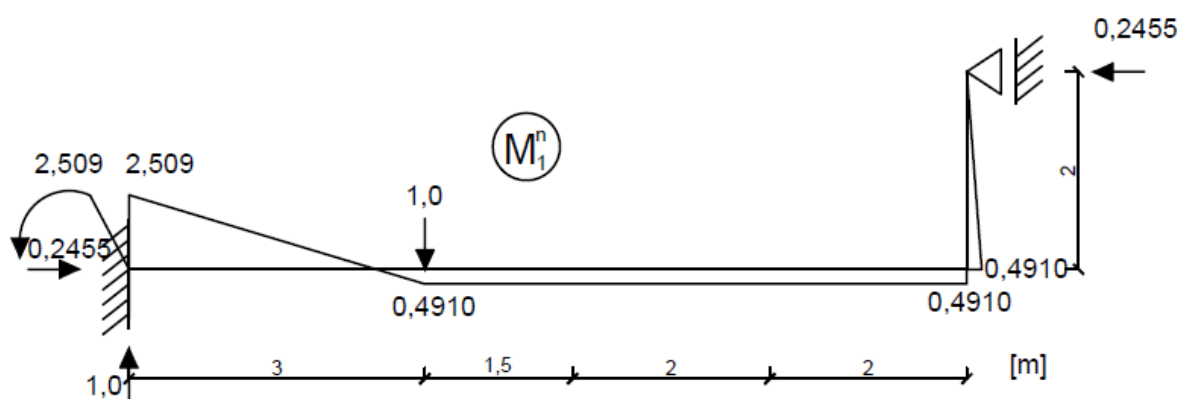
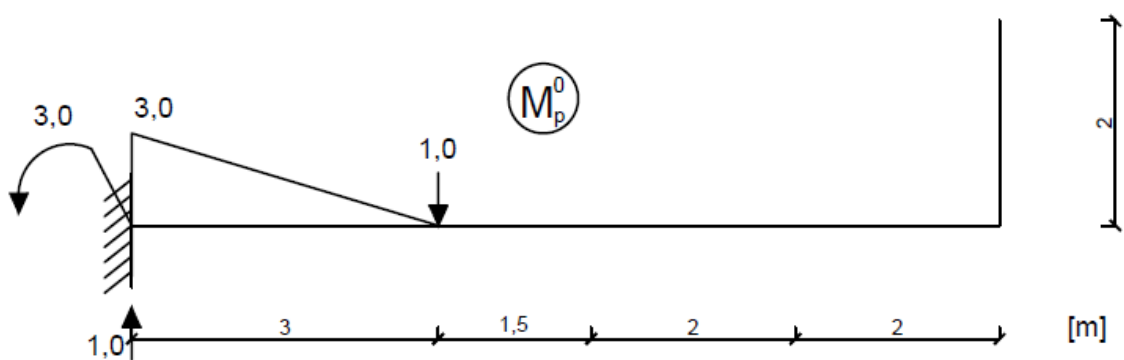
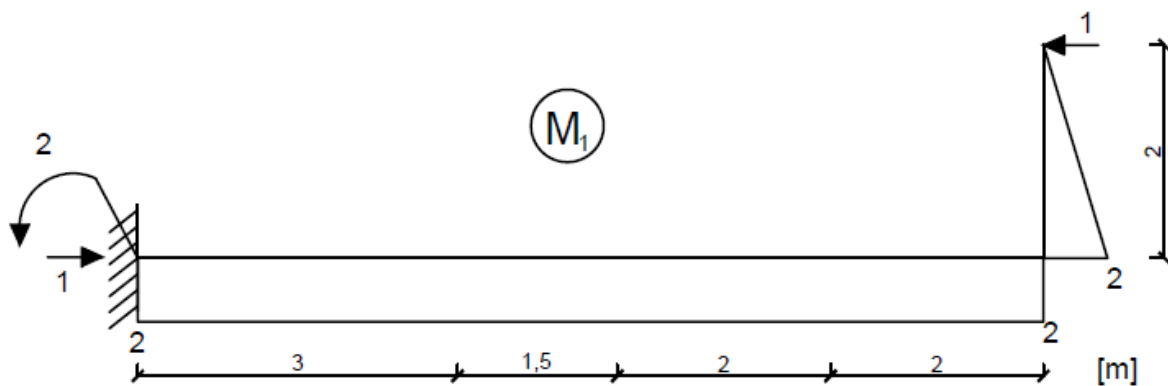
$$\begin{vmatrix} 1 - 2,5\delta'_{11}\lambda & -3,2\delta'_{12}\lambda & -4\delta'_{13}\lambda \\ -2,5\delta'_{21}\lambda & 1 - 3,2\delta'_{22}\lambda & -4\delta'_{23}\lambda \\ -2,5\delta'_{31}\lambda & -3,2\delta'_{32}\lambda & 1 - 4\delta'_{33}\lambda \end{vmatrix} = 0$$

Wyznaczenie wykresu od siły $P=1,0$ po kierunku q_1 metodą sił:

$$\delta_{11} = \frac{1}{EI} (2 \cdot 8,5 \cdot 2 + 2 \cdot 2 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 2) = \frac{110}{3} \frac{1}{EI}$$

$$\delta_{1p} = \frac{1}{EI} \left(-3 \cdot \frac{1}{2} \cdot 3 \cdot 2 \right) = -9 \frac{1}{EI}$$

$$X_1 = -\frac{\delta_{1p}}{\delta_{11}} = 9 \cdot \frac{3}{110} = 0,2455$$

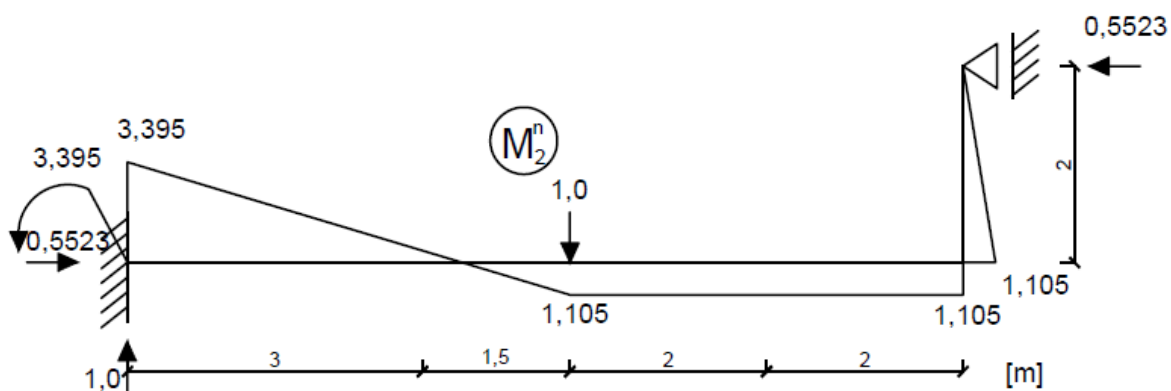
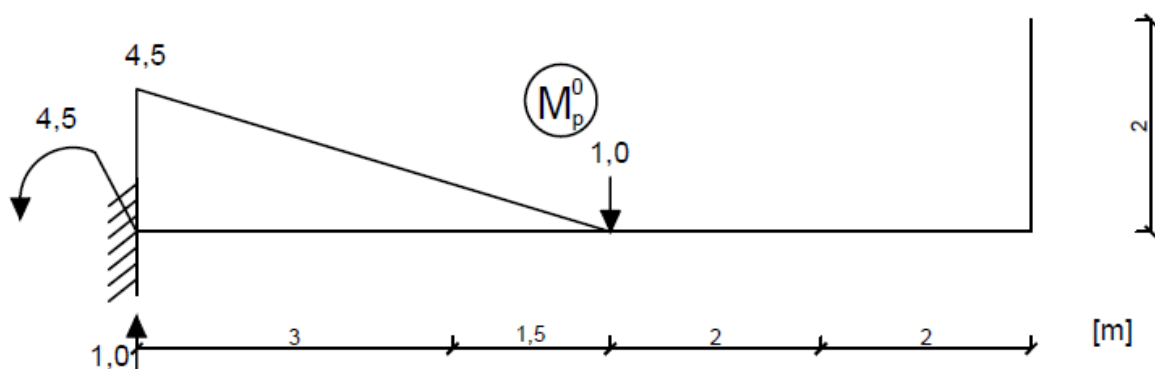
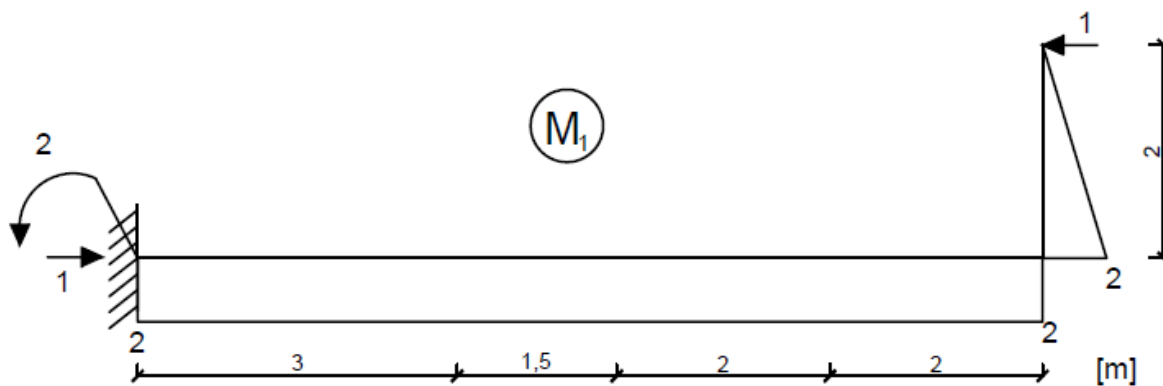


Wyznaczenie wykresu od siły $P=1,0$ po kierunku q_2 metodą sił:

$$\delta_{11} = \frac{1}{EI} (2 \cdot 8,5 \cdot 2 + 2 \cdot 2 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 2) = \frac{110}{3} \frac{1}{EI}$$

$$\delta_{1p} = \frac{1}{EI} (-4,5 \cdot \frac{1}{2} \cdot 4,5 \cdot 2) = -20,25 \frac{1}{EI}$$

$$X_2 = -\frac{\delta_{1p}}{\delta_{11}} = 20,25 \cdot \frac{3}{110} = 0,5523$$

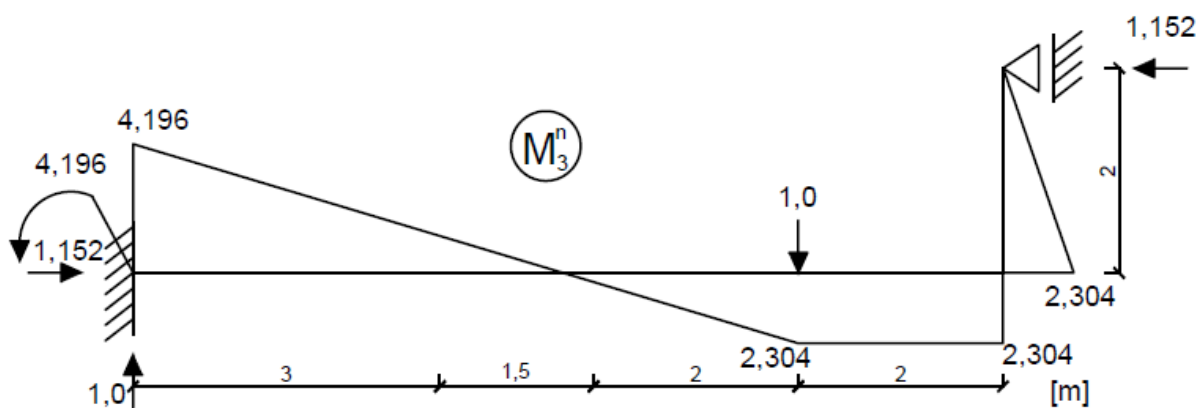
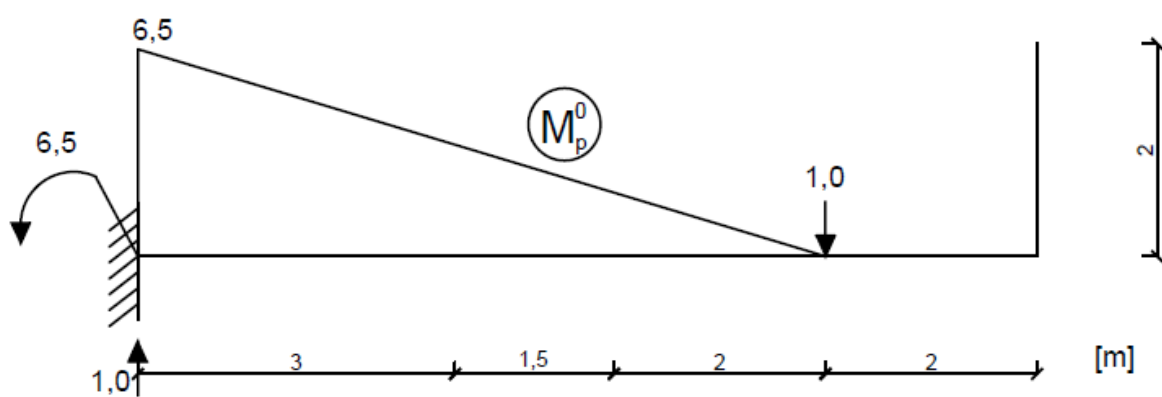
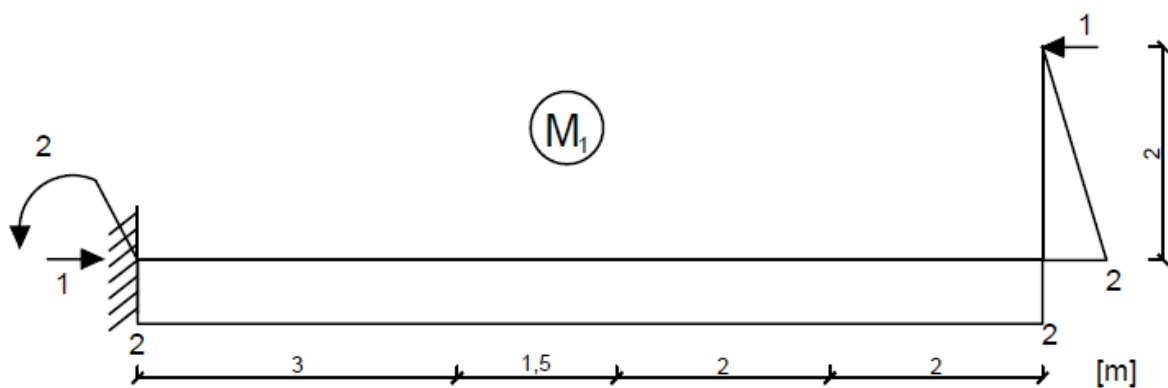


Wyznaczenie wykresu od Wyznaczenie wykresu od siły $P=1,0$ po kierunku q_3

$$\delta_{11} = \frac{1}{EI} (2 \cdot 8,5 \cdot 2 + 2 \cdot 2 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 2) = \frac{110}{3} \frac{1}{EI}$$

$$\delta_{1p} = \frac{1}{EI} (-6,5 \cdot \frac{1}{2} \cdot 6,5 \cdot 2) = -42,25 \frac{1}{EI}$$

$$X_3 = -\frac{\delta_{1p}}{\delta_{11}} = 42,25 \cdot \frac{3}{110} = 1,152$$



Współczynniki δ_{ik}' z układu równań ruchu:

$$\delta_{ik}' = \sum \int M_i M_k dx$$

$$\delta'_{11} = \int M_1^0 \cdot M_1^n dx = 2,51 \cdot 3 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 3 - 0,49 \cdot 3 \cdot \frac{1}{2} \cdot \frac{1}{3} \cdot 3 = 6,795$$

$$\delta'_{12} = \int M_1^0 \cdot M_2^n dx = 3,396 \cdot 3 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 3 + 0,396 \cdot 3 \cdot \frac{1}{2} \cdot \frac{1}{3} \cdot 3 = 10,782$$

$$\delta'_{22} = \int M_2^0 \cdot M_2^n dx = 3,396 \cdot 4,5 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 4,5 - 1,104 \cdot 4,5 \cdot \frac{1}{2} \cdot \frac{1}{3} \cdot 4,5 = 19,197$$

$$\delta'_{23} = \int M_2^0 \cdot M_3^n dx = 4,196 \cdot 4,5 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 4,5 - 0,304 \cdot 4,5 \cdot \frac{1}{2} \cdot \frac{1}{3} \cdot 4,5 = 27,297$$

$$\delta'_{33} = \int M_3^0 \cdot M_3^n dx = 4,196 \cdot 6,5 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 6,5 - 2,304 \cdot 6,5 \cdot \frac{1}{2} \cdot \frac{1}{3} \cdot 6,5 = 42,87$$

$$\delta'_{13} = \int M_1^0 \cdot M_3^n dx = 4,196 \cdot 3 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 3 + 1,196 \cdot 3 \cdot \frac{1}{2} \cdot \frac{1}{3} \cdot 3 = 14,382$$

$$\begin{vmatrix} 1 - 16,988\lambda & -34,502\lambda & -57,528\lambda \\ -26,955\lambda & 1 - 61,430\lambda & -109,188\lambda \\ -35,955\lambda & -87,350\lambda & 1 - 171,48\lambda \end{vmatrix} = 0$$

$$(1 - 16,988\lambda)(1 - 61,430\lambda)(1 - 171,48\lambda) - 135451\lambda^3 - 135450\lambda^3 - (1 - 61,430\lambda)2068,419\lambda^2 - (1 - 16,988\lambda)9537,572\lambda^2 - (1 - 171,48\lambda)930,001\lambda^2 = 0$$

$$(1 - 78,418\lambda + 1043,573\lambda^2)(1 - 171,48\lambda) - 135451\lambda^3 - 135450\lambda^3 - 2068,419\lambda^2 + 127063\lambda^3 - 9537,572\lambda^2 + 162024\lambda^3 - 930,001\lambda^2 + 159477\lambda^3 = 0$$

$$1 - 78,418\lambda + 1043,573\lambda^2 - 171,481\lambda + 13447,119\lambda^2 - 178951,898\lambda^3 - 135451\lambda^3 - 135450\lambda^3 - 2068,419\lambda^2 + 127063\lambda^3 - 9537,572\lambda^2 + 162024\lambda^3 - 930,001\lambda^2 + 159477\lambda^3 = 0$$

$$1 - 249,899\lambda + 1954,7\lambda^2 - 1288,898\lambda^3 = 0$$

$$\lambda_1 = 0,004135$$

$$\lambda_2 = 0,136353$$

$$\lambda_3 = 1,376079$$

$$\omega = \sqrt{\frac{\lambda EI}{m}}$$

$$\omega_3 = \sqrt{\frac{1,376079 \cdot 6273000}{100}} = 293,805 \frac{rad}{s}$$

$$\omega_2 = \sqrt{\frac{0,136353 \cdot 6273000}{100}} = 92,485 \frac{rad}{s}$$

$$\omega_1 = \sqrt{\frac{0,004135 \cdot 6273000}{100}} = 16,106 \frac{rad}{s}$$

$$\begin{cases} A_1(1 - 16,988\lambda) - A_2 34,502\lambda - A_3 57,528\lambda = 0 \\ -A_1 26,955\lambda + A_2(1 - 61,430\lambda) - A_3 109,188\lambda = 0 \\ -A_1 35,955\lambda - A_2 87,350\lambda + A_3(1 - 171,48\lambda) = 0 \end{cases}$$

$$\begin{cases} A_1(1 - 16,988\lambda) - A_2 34,502\lambda - A_3 57,528\lambda = 0 \\ -A_1 26,955\lambda + A_2(1 - 61,430\lambda) - A_3 109,188\lambda = 0 \end{cases}$$

I postać drgań własnych:

$$\lambda_1 = 0,004135$$

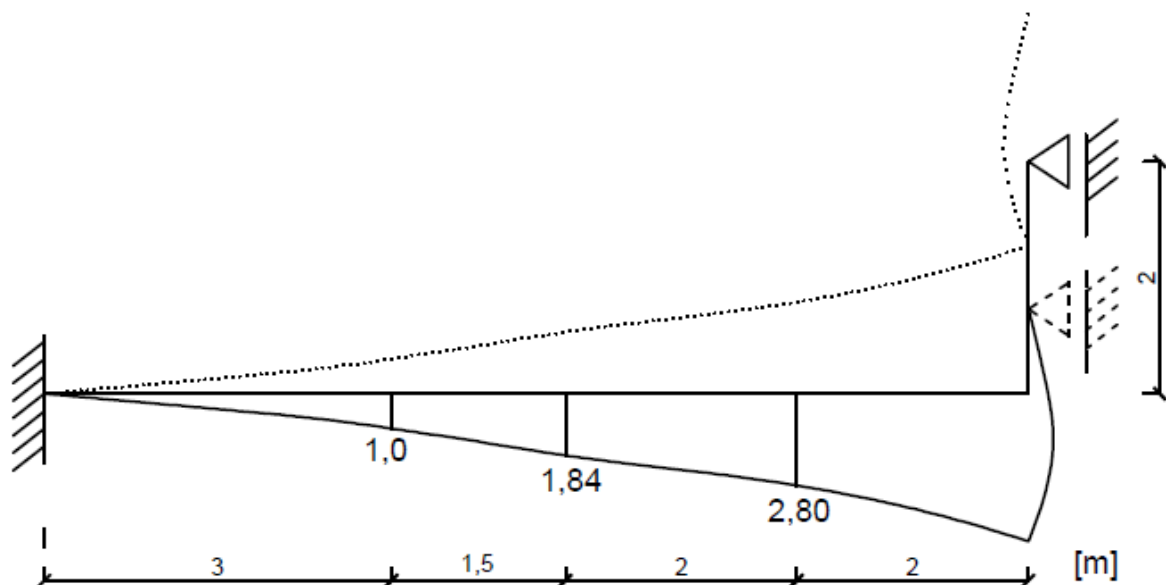
$$A_1 = 1,0$$

$$\begin{cases} 0,930 - A_2 0,143 - A_3 0,238 = 0 \\ -0,111 + A_2 0,746 - A_3 0,451 = 0 \end{cases}$$

$$A_1 = 1,0$$

$$A_2 = 1,842$$

$$A_3 = 2,801$$



II postać drgań własnych:

$$\lambda_2 = 0,136353$$

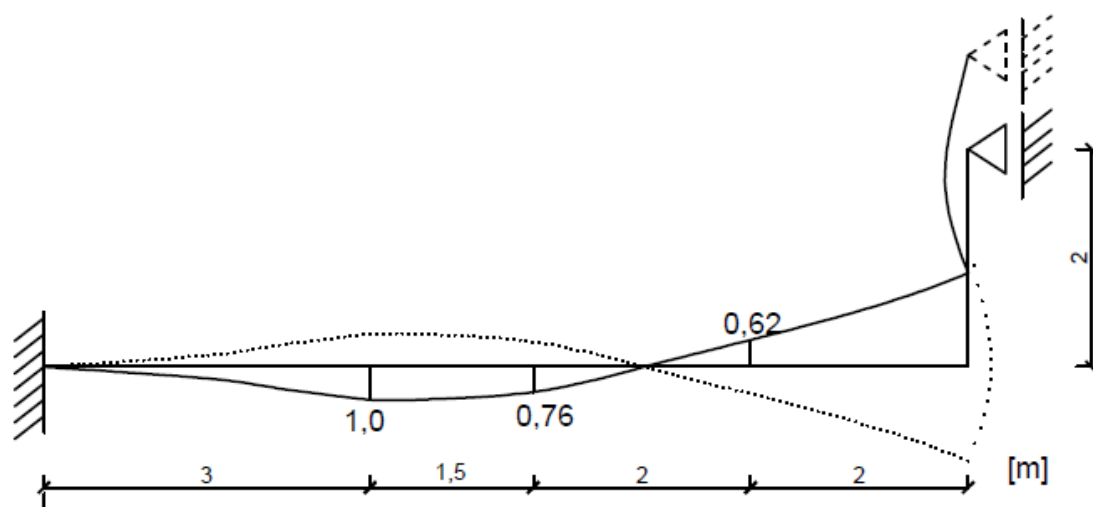
$$A_1 = 1,0$$

$$\begin{cases} -1,316 - A_2 4,704 - A_3 7,844 = 0 \\ -3,675 - A_2 7,376 - A_3 14,888 = 0 \end{cases}$$

$$A_1 = 1,0$$

$$A_2 = 0,7584$$

$$A_3 = -0,6226$$



III postać drgań własnych:

$$\lambda_3 = 1,376079$$

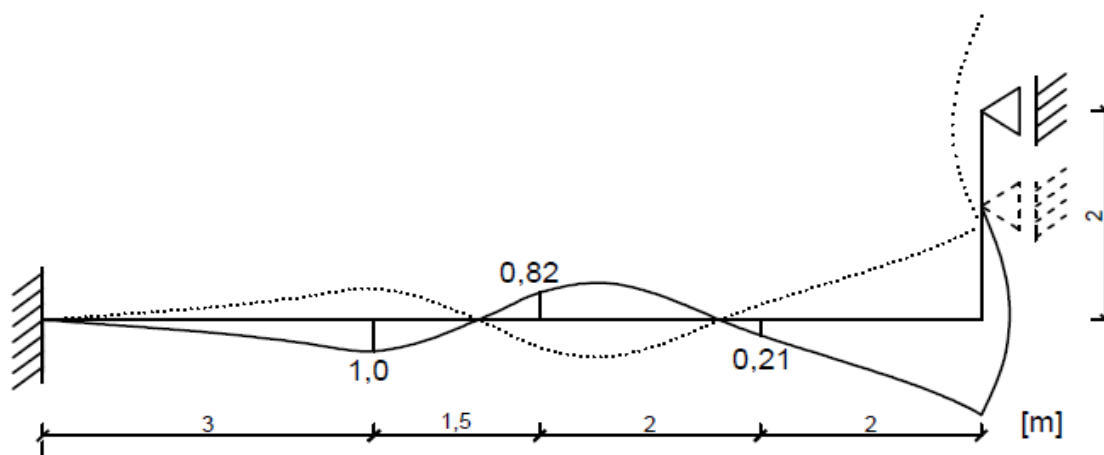
$$A_1 = 1,0$$

$$\begin{cases} -22,377 - A_2 47,477 - A_3 79,163 = 0 \\ -37,092 - A_2 83,533 - A_3 150,251 = 0 \end{cases}$$

$$A_1 = 1,0$$

$$A_2 = -0,8178$$

$$A_3 = 0,2078$$



Sprawdzenie ortogonalności:

$$\sum A_i^{II} \cdot m_i \cdot A_i^I = 1 \cdot 2,5 \cdot 1 + 0,7584 \cdot 3,2 \cdot 1,842 + (-0,6226) \cdot 4 \cdot 2,801 = -0,005 \approx 0$$

$$\sum A_i^{III} \cdot m_i \cdot A_i^I = 1 \cdot 2,5 \cdot 1 + (-0,8178) \cdot 3,2 \cdot 1,842 + 0,2078 \cdot 4 \cdot 2,801 = 0,008 \approx 0$$

$$\sum A_i^{III} \cdot m_i \cdot A_i^{II} = 1 \cdot 2,5 \cdot 1 + (-0,8178) \cdot 3,2 \cdot 0,7584 + 0,2078 \cdot 4 \cdot (-0,6226) = -0,002 \approx 0$$

3. Drgania wymuszone:

$$\begin{cases} A_1(1 - 2,5\delta_{11} p^2 m) - A_2 3,2\delta_{12} p^2 m - A_3 4\delta_{13} p^2 m = P\delta_{12} \\ -A_1 2,5\delta_{21} p^2 m + A_2(1 - 3,2\delta_{22} p^2 m) - A_3 4\delta_{23} p^2 m = P\delta_{22} \\ -A_1 2,5\delta_{31} p^2 m - A_2 3,2\delta_{32} p^2 m + A_3(1 - 4\delta_{33} p^2 m) = P\delta_{32} \end{cases}$$

$$\frac{p^2}{EI_0} = \frac{65,97^2}{6273000}$$

$$\begin{cases} -A_1 0,1785 - A_2 2,3937 - A_3 3,9911 = 0,0438 \\ -A_1 1,8701 - A_2 3,2619 - A_3 7,5752 = 0,0780 \\ -A_1 2,4945 - A_2 6,0601 - A_3 10,8968 = 0,1743 \end{cases}$$

$$A_1 = -0,039343 \text{ m}$$

$$A_2 = -0,051022 \text{ m}$$

$$A_3 = 0,021386 \text{ m}$$

4. Obwiednia momentów dynamicznych:

$$B_1 = -m_1 \ddot{q}_1 = -m_1(-A_1 p^2 \sin(pt)) = m_1(A_1 p^2 \sin(pt)) = 250 \cdot (-0,039343) \cdot 65,97^2 \cdot \sin(pt)$$

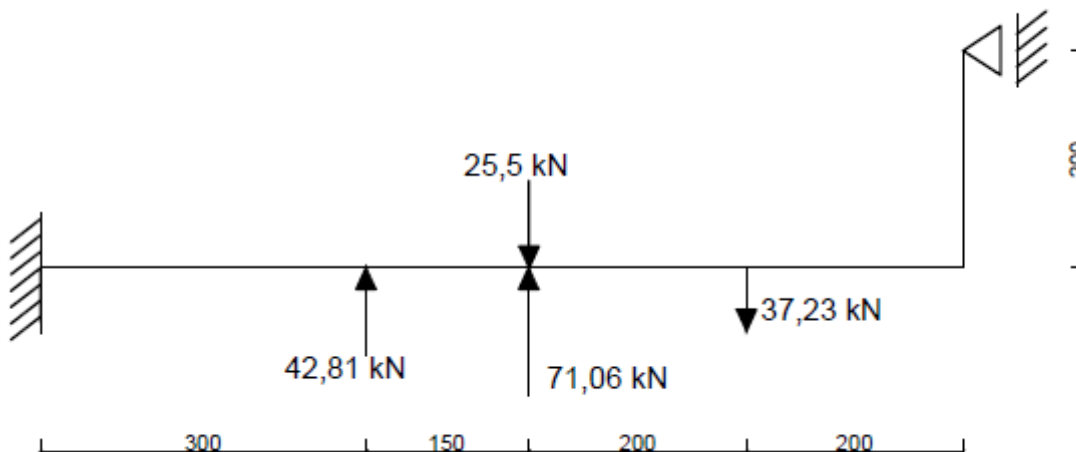
$$\begin{aligned} \text{dla } \sin(pt) = 1 & \quad B_1 = -42805,58 \text{ N} = -42,81 \text{ kN} \\ \text{dla } \sin(pt) = -1 & \quad B_1 = 42805,58 \text{ N} = 42,81 \text{ kN} \end{aligned}$$

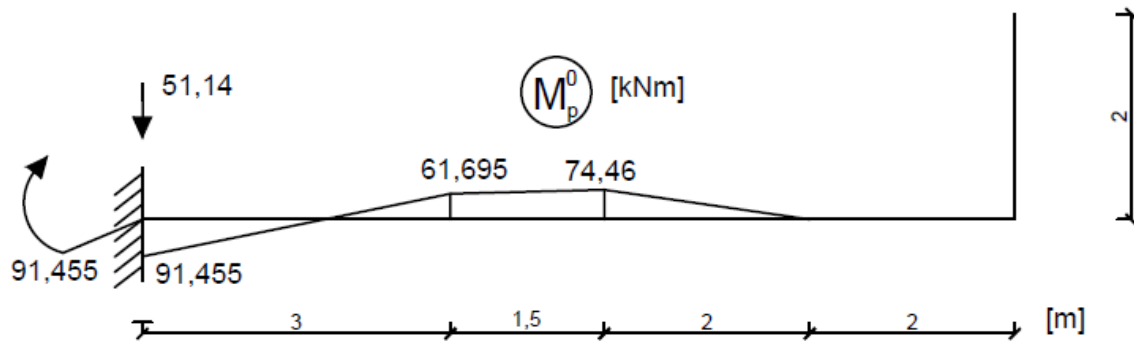
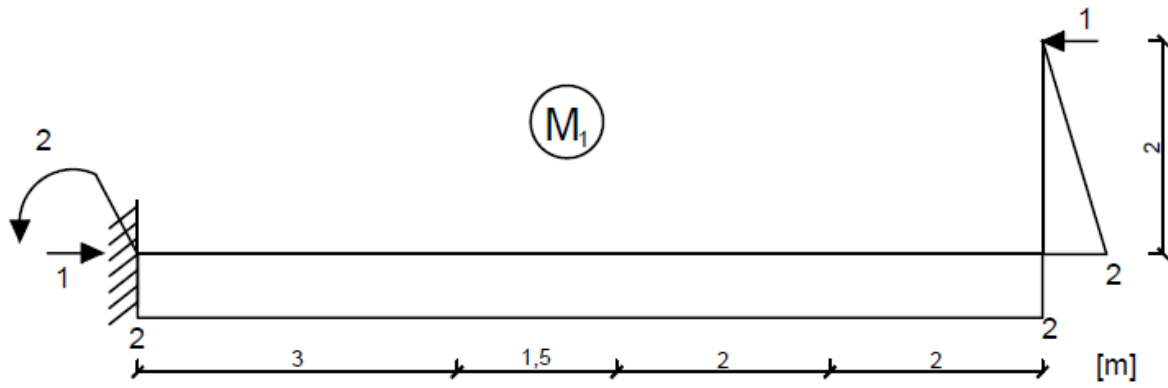
$$B_2 = -m_2 \ddot{q}_2 = -m_2(-A_2 p^2 \sin(pt)) = m_2(A_2 p^2 \sin(pt)) = 320 \cdot (-0,051022) \cdot 65,97^2 \cdot \sin(pt)$$

$$\begin{aligned} \text{dla } \sin(pt) = 1 & \quad B_2 = -71055,95 \text{ N} = -71,06 \text{ kN} \\ \text{dla } \sin(pt) = -1 & \quad B_2 = 71055,95 \text{ N} = 71,06 \text{ kN} \end{aligned}$$

$$B_3 = -m_3 \ddot{q}_3 = -m_3(-A_3 p^2 \sin(pt)) = m_3(A_3 p^2 \sin(pt)) = 400 \cdot 0,021386 \cdot 65,97^2 \cdot \sin(pt)$$

$$\begin{aligned} \text{dla } \sin(pt) = 1 & \quad B_3 = 37229,10 \text{ N} = 37,23 \text{ kN} \\ \text{dla } \sin(pt) = -1 & \quad B_3 = -37229,10 \text{ N} = -37,23 \text{ kN} \end{aligned}$$

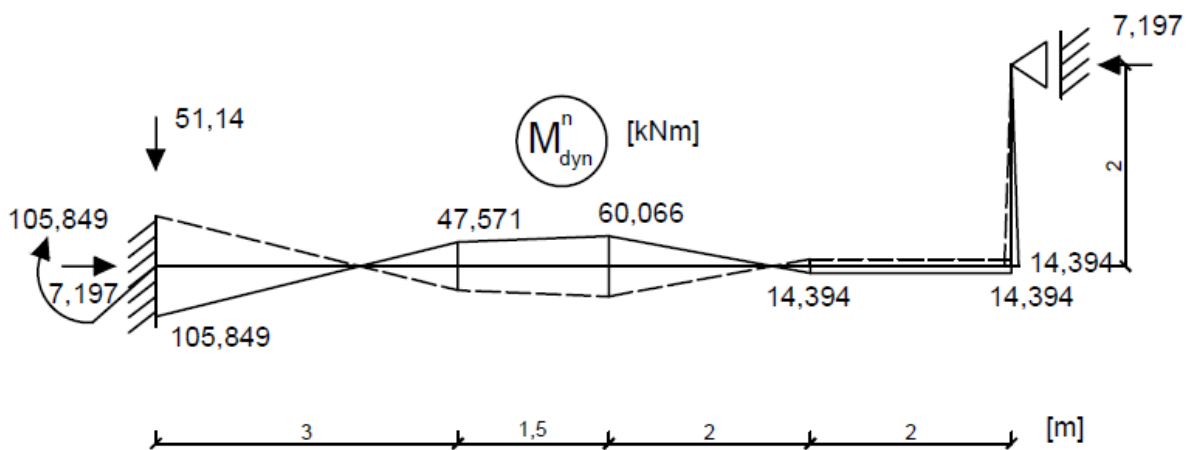




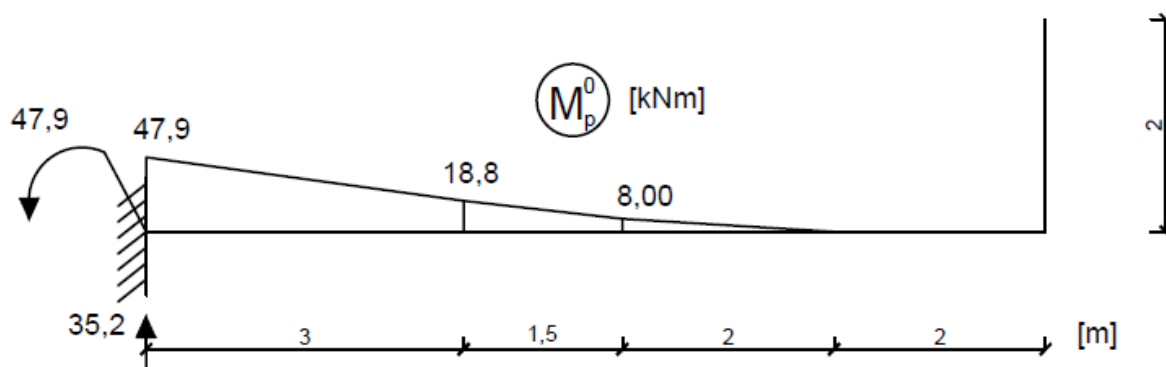
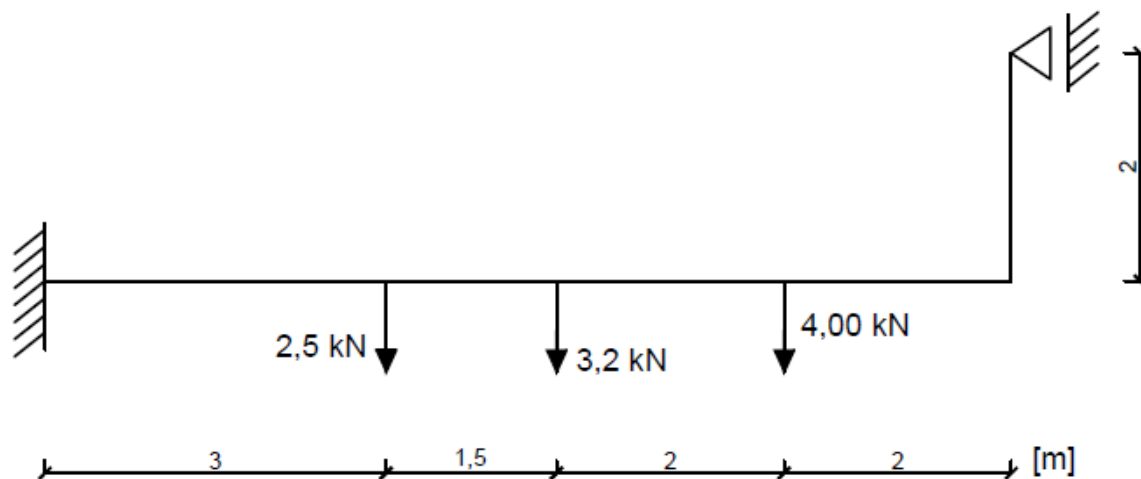
$$\delta_{11} = \frac{1}{EI} (2 \cdot 8,5 \cdot 2 + 2 \cdot 2 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 2) = \frac{110}{3} \frac{1}{EI}$$

$$\delta_{1p} = \frac{1}{EI} (91,455 \cdot \frac{1}{2} \cdot 3 - 61,695 \cdot \frac{1}{2} \cdot 3 - 61,695 \cdot \frac{1}{2} \cdot 1,5 - 74,46 \cdot (1,5 + 2) \cdot \frac{1}{2}) \cdot 2 = -263,873 \frac{1}{EI}$$

$$X = -\frac{\delta_{1p}}{\delta_{11}} = 263,873 \cdot \frac{3}{110} = 7,197 \text{ kN}$$



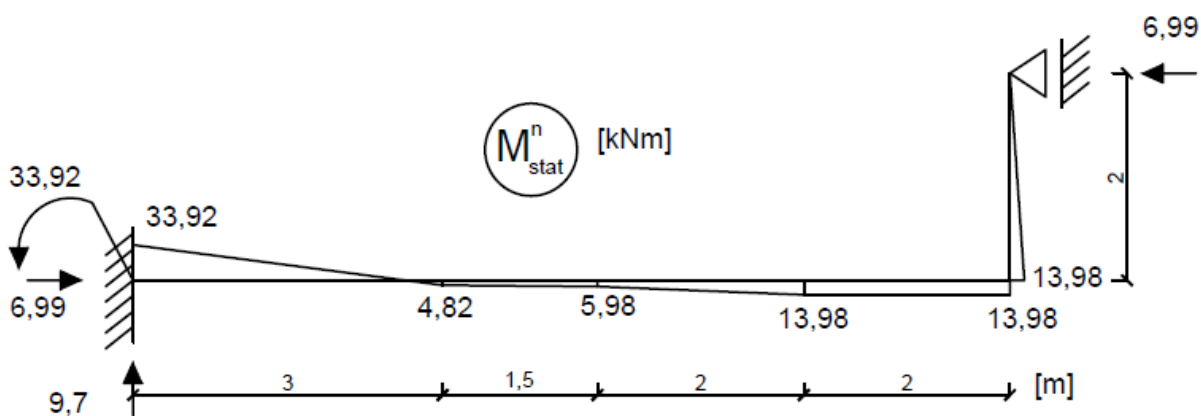
5. Rozkład momentów zginających of obciążenia statycznego (ciężar własny mas, ciężar własny prętów pominięto):



$$\delta_{11} = \frac{1}{EI} (2 \cdot 8,5 \cdot 2 + 2 \cdot 2 \cdot \frac{1}{2} \cdot \frac{2}{3} \cdot 2) = \frac{110}{3} \frac{1}{EI}$$

$$\delta_{1p} = \frac{1}{EI} \left[- \left(47,9 \cdot \frac{1}{2} \cdot 3 + 18,8 \cdot \frac{1}{2} \cdot 3 + 18,8 \cdot \frac{1}{2} \cdot 1,5 + 8,0 \cdot (1,5 + 2) \cdot \frac{1}{2} \right) \right] \cdot 2 = -256,3 \frac{1}{EI}$$

$$X = - \frac{\delta_{1p}}{\delta_{11}} = 256,3 \cdot \frac{3}{110} = 6,99 \text{ kN}$$



6. Maksymalne naprężenia normalne:

$$\sigma = 1,2 \cdot \frac{M_{stat}}{W} + 5,0 \frac{M_{dyn}}{W} = 1,2 \cdot \frac{3392}{278} + 5,0 \cdot \frac{10584,9}{278} = 205,12 \frac{kN}{cm^2}$$

$$\sigma_{dop} = 21,5 \frac{kN}{cm^2} < \sigma = 205,12 \frac{kN}{cm^2}$$

Przekrój nie spełnia warunku nośności.