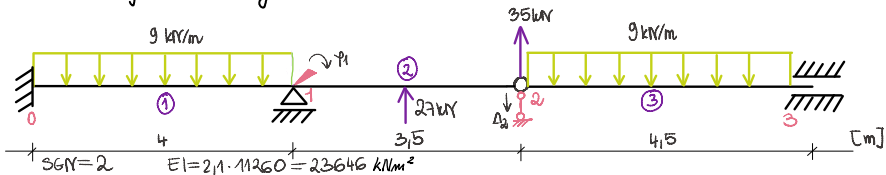




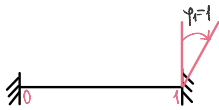
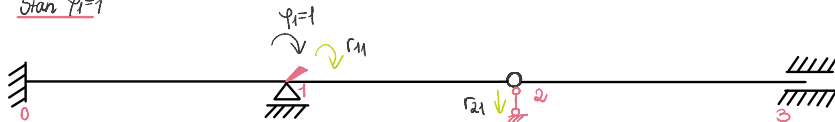
Ćwiczenie nr 1  
Metoda Przemieszczeń  
Belka

Prrowadzący: mgr. inż. Aneta Kowor  
Autor: Kamelia Nowak  
Nr indeksu: 152258  
Semestr/rok: IV / 2022/2023

# Układ podstawowy:

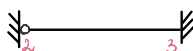


## Stan $\varphi_1=1$



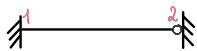
$$M_{01} = \frac{2EI}{4} \cdot 1 = 0,5EI$$

$$M_{40} = \frac{2EI}{4} \cdot 2 = EI$$



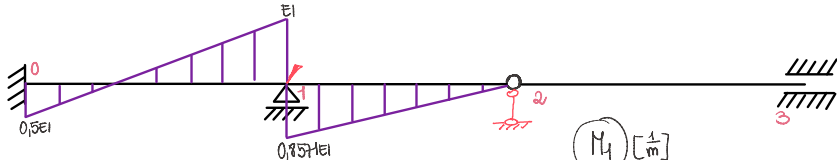
$$M_{20} = 0$$

$$M_{32} = 0$$

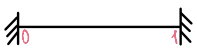
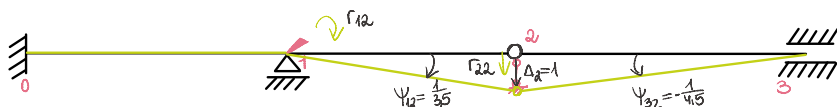


$$M_{12} = \frac{3EI}{3,5} \cdot 1 = 0,857EI$$

$$M_{21} = 0$$

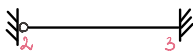


## Stan $\Delta_2=1$



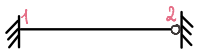
$$M_{01} = 0$$

$$M_{40} = 0$$



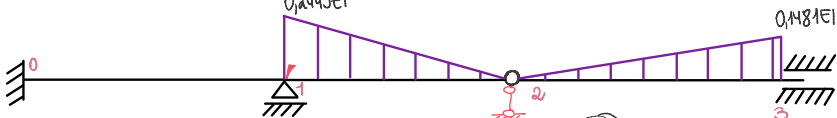
$$M_{20} = 0$$

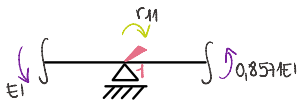
$$M_{32} = \frac{3EI}{4,5} \cdot \frac{1}{4,5} = 0,1481EI$$



$$M_{12} = \frac{3EI}{3,5} \cdot \left(-\frac{1}{3,5}\right) = -0,2449EI$$

$$M_{21} = 0$$

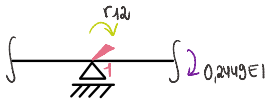




$$\sum M^{(i)} = 0$$

$$r_{11} - EI - 0,857EI = 0$$

$$\underline{r_{11} = 1,857EI}$$



$$\sum M^{(i)} = 0$$

$$r_{12} + 0,2449EI = 0$$

$$\underline{r_{12} = -0,2449EI}$$

RPN

$$r_{21} \cdot \bar{1} + 0,857EI \cdot \frac{\bar{1}}{3\bar{5}} = 0$$

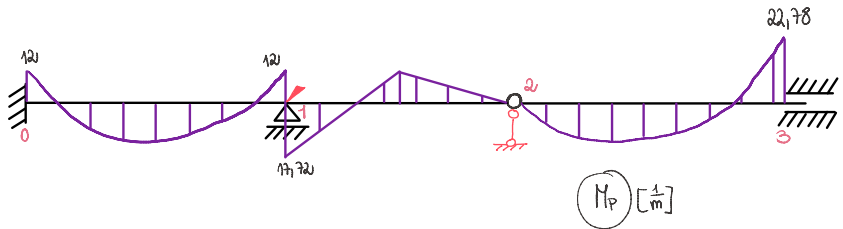
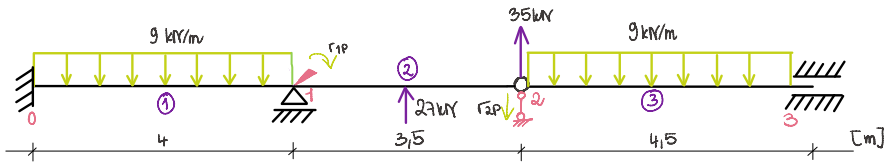
$$\underline{r_{21} = 0,2449EI}$$

$$r_{22} \cdot \bar{1} - 0,2449EI \cdot \frac{\bar{1}}{3\bar{5}} + 0,1481EI \cdot \left(-\frac{\bar{1}}{4\bar{5}}\right) = 0$$

$$\underline{r_{22} = 0,1029EI}$$

$$K = \begin{bmatrix} 1,857EI & -0,2449EI \\ -0,2449EI & 0,1029EI \end{bmatrix}$$

Stan P



$$\sum M^{(i)} = 0$$

$$r_{1P} - 12 - 17,72 = 0$$

$$\underline{r_{1P} = 29,72 \text{ kNm}}$$

RPN

$$r_{2P} \cdot \bar{1} + 17,72 \cdot \frac{\bar{1}}{3\bar{5}} + 22,78 \cdot \left(\frac{\bar{1}}{4\bar{5}}\right) - 27 \cdot \bar{0}\bar{5} - 35 \cdot \bar{1} + 9 \cdot 4\bar{5} \cdot \bar{0}\bar{5} = 0$$

$$\underline{r_{2P} = 28,25 \text{ kN}}$$

# URK

$$\begin{cases} r_{11}\varphi_1 + r_{12}A_2 + r_{1p} = 0 \\ r_{21}\varphi_1 + r_{22}A_2 + r_{2p} = 0 \end{cases}$$

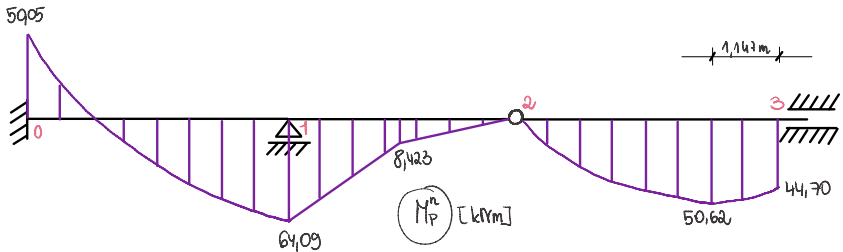
$$K = \begin{bmatrix} 1,857EI & -0,2449EI \\ -0,2449EI & 0,1029EI \end{bmatrix}$$

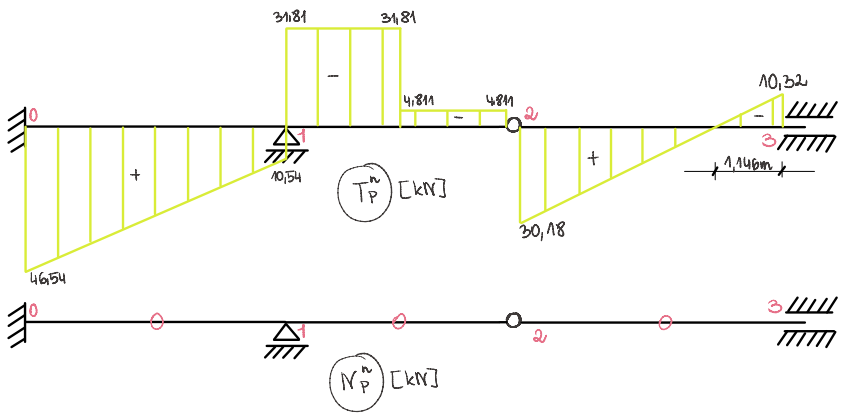
$$\begin{cases} 1,857\varphi_1 - 0,2449A_2 + 29,72 = 0 \\ -0,2449\varphi_1 + 0,1029A_2 + 28,25 = 0 \end{cases}$$

$$\begin{cases} \varphi_1 = -\frac{76,09}{EI} = -0,1844^\circ \\ A_2 = -\frac{455,64}{EI} = -0,01927 \text{ m} \end{cases}$$

$$M_{ik}^n = M_{ik}^{(1)}\varphi_1 + M_{ik}^{(2)}A_2 + M_{ik}^{(p)}$$

ik	$M_{ik}^{(1)}$	$M_{ik}^{(2)}$	$M_{ik}^{(p)}$	$M_{ik}^{(n)}$ [kNm]
01	0,5	0	-12	-50,09
10	1	0	12	-64,09
12	0,8571	-0,2449	77,72	64,09
32	0	0,1481	22,78	-44,70



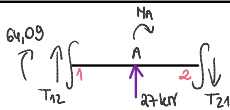


$$\sum M^{(0)} = 9 \cdot 4 \cdot 2 + T_{10} \cdot 4 - 64,09 - 50,05 = 0$$

$$T_{10} = 10,54 \text{ kN}$$

$$\sum H^{(0)} = -9 \cdot 4 \cdot 2 + T_{01} \cdot 4 - 64,09 - 50,05 = 0$$

$$T_{01} = 46,54 \text{ kN}$$



$$\sum M^{(1)} = 64,09 - 27 \cdot \frac{3,5}{2} + T_{21} \cdot 3,5 = 0$$

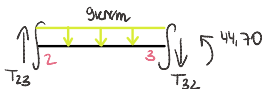
$$T_{21} = -4,811 \text{ kN}$$

$$\sum H^{(1)} = 64,09 + T_{12} \cdot 3,5 + 27 \cdot \frac{3,5}{2} = 0$$

$$T_{12} = -31,81 \text{ kN}$$

$$\sum M^{(2)} = 64,09 - 31,81 \cdot \frac{3,5}{2} + M_A = 0$$

$$M_A = -8,423 \text{ kNm}$$



$$\sum M^{(2)} = 9 \cdot 4,5 \cdot \frac{4,5}{2} - 44,70 + T_{32} \cdot 4,5 = 0$$

$$T_{32} = -10,32 \text{ kN}$$

$$\sum H^{(2)} = -9 \cdot 4,5 \cdot \frac{4,5}{2} - 44,70 + T_{23} \cdot 4,5 = 0$$

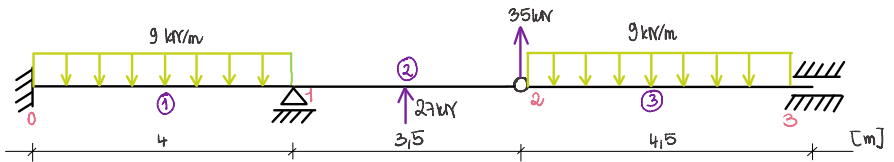
$$T_{23} = 39,18 \text{ kN}$$

$$T(x) = -9 \cdot x + 10,32 = 0$$

$$x = 1,147 \text{ m}$$

$$\sum M^{(1147)} = M_{\text{EXT}} + 9 \cdot 1,147 \cdot \frac{1,147}{2} - 44,70 - 10,32 \cdot 1,147 = 0$$

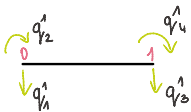
$$M_{\text{EXT}} = 50,62 \text{ kNm}$$



$$EI = \text{const} \Rightarrow EI = 2,1 \cdot 11260 = 23646$$

### Macierz sztywności

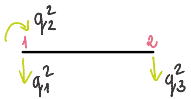
①



$$q_1 = \begin{bmatrix} q_1^1 \\ q_1^2 \\ q_1^3 \\ q_1^4 \end{bmatrix}$$

$$K_1 = \begin{bmatrix} \frac{12EI}{l^3} & \frac{6EI}{l^2} & -\frac{12EI}{l^3} & \frac{6EI}{l^2} \\ \frac{6EI}{l^2} & \frac{4EI}{l} & -\frac{6EI}{l^2} & \frac{2EI}{l} \\ -\frac{12EI}{l^3} & -\frac{6EI}{l^2} & \frac{12EI}{l^3} & -\frac{6EI}{l^2} \\ \frac{6EI}{l^2} & \frac{2EI}{l} & -\frac{6EI}{l^2} & \frac{4EI}{l} \end{bmatrix} = EI \begin{bmatrix} 0,1875 & 0,3750 & -0,1875 & 0,3750 \\ 0,3750 & 1 & -0,3750 & 0,5 \\ -0,1875 & -0,3750 & 0,1875 & -0,3750 \\ 0,3750 & 0,5 & -0,3750 & 1 \end{bmatrix}$$

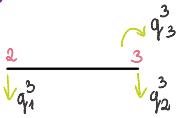
②



$$q_2 = \begin{bmatrix} q_2^1 \\ q_2^2 \\ q_2^3 \\ q_2^4 \end{bmatrix}$$

$$K_2 = \begin{bmatrix} \frac{3EI}{l^3} & \frac{3EI}{l^2} & -\frac{3EI}{l^3} & 0 \\ \frac{3EI}{l^2} & \frac{3EI}{l} & -\frac{3EI}{l^2} & 0 \\ \frac{3EI}{l^3} & -\frac{3EI}{l^2} & \frac{3EI}{l^3} & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} = EI \begin{bmatrix} 0,06997 & 0,2449 & -0,06997 & 0 \\ 0,2449 & 0,8571 & -0,2449 & 0 \\ -0,06997 & -0,2449 & 0,06997 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

③

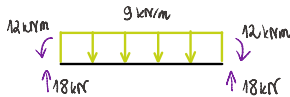
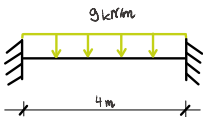


$$q_2 = \begin{bmatrix} q_1^3 \\ q_2^3 \\ q_3^3 \end{bmatrix}$$

$$K_3 = \begin{bmatrix} \frac{3EI}{l^3} & -\frac{3EI}{l^3} & \frac{3EI}{l^2} \\ \frac{3EI}{l^3} & \frac{3EI}{l^3} & -\frac{3EI}{l^2} \\ \frac{3EI}{l^2} & -\frac{3EI}{l^2} & \frac{3EI}{l} \end{bmatrix} = EI \begin{bmatrix} 0,03292 & -0,03292 & 0,1481 \\ -0,03292 & 0,03292 & -0,1481 \\ 0,1481 & -0,1481 & 0,6667 \end{bmatrix}$$

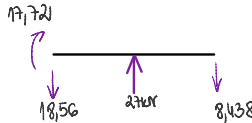
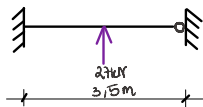
Nektory reakcji przynależnych od obciążenia przedowego

①



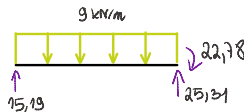
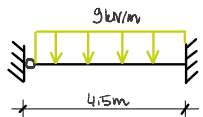
$$R_{01} = \begin{bmatrix} -18 \\ -12 \\ -18 \\ 12 \end{bmatrix}$$

②



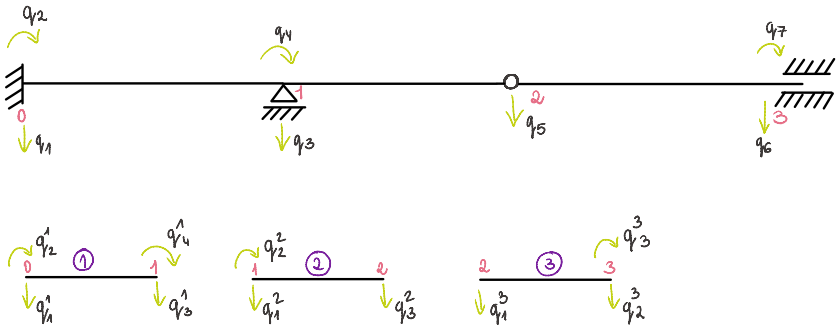
$$R_{02} = \begin{bmatrix} 18,56 \\ 17,72 \\ 8,438 \end{bmatrix}$$

③



$$R_{03} = \begin{bmatrix} -15,19 \\ -25,31 \\ 22,78 \end{bmatrix}$$

## Przemieszczenia w układzie globalnym



## Tablica powiązań

Nr elementu	Numer przemieszczeń				E-LOGARUNE
	1	2	3	4	
1	1	2	3	4	
2	3	4	5	-	
3	5	6	7	-	

## Agregacja macierzy sztywności

$$K_1 = EI \begin{bmatrix} 0,1875 & 0,3750 & -0,1875 & 0,6750 \\ 0,3750 & 1 & -0,3750 & 0,5 \\ -0,1875 & -0,3750 & 0,1875 & -0,3750 \\ 0,6750 & 0,5 & -0,3750 & 1 \end{bmatrix}$$

$$K_2 = EI \begin{bmatrix} 0,06997 & 0,2449 & -0,06997 \\ 0,2449 & 0,8571 & -0,2449 \\ -0,06997 & -0,2449 & 0,06997 \end{bmatrix}$$

$$K_3 = EI \begin{bmatrix} 0,03292 & -0,03292 & 0,1481 \\ -0,03292 & 0,03292 & -0,1481 \\ 0,1481 & -0,1481 & 0,6667 \end{bmatrix}$$



$$\underline{K} = E I \begin{bmatrix}
 0,1875 & 0,3750 & -0,1875 & 0,3750 & 0 & 0 & 0 \\
 0,3750 & 1 & -0,3750 & 0,5 & 0 & 0 & 0 \\
 -0,1875 & -0,3750 & 0,1875 + 0,06997 & -0,3750 + 0,2449 & -0,06997 & 0 & 0 \\
 0,3750 & 0,5 & -0,3750 + 0,2449 & 1 + 0,8571 & -0,2449 & 0 & 0 \\
 0 & 0 & -0,06997 & -0,2449 & 0,06997 + 0,03292 & -0,03292 & 0,1481 \\
 0 & 0 & 0 & 0 & -0,03292 & 0,03292 & -0,1481 \\
 0 & 0 & 0 & 0 & 0,1481 & -0,1481 & 0,6667
 \end{bmatrix}$$

$$\underline{K} = E I \begin{bmatrix}
 0,1875 & 0,3750 & -0,1875 & 0,3750 & 0 & 0 & 0 \\
 0,3750 & 1 & -0,3750 & 0,5 & 0 & 0 & 0 \\
 -0,1875 & -0,3750 & 0,2575 & -0,1301 & -0,06997 & 0 & 0 \\
 0,3750 & 0,5 & -0,1301 & 1,857 & -0,2449 & 0 & 0 \\
 0 & 0 & -0,06997 & -0,2449 & 0,1029 & -0,03292 & 0,1481 \\
 0 & 0 & 0 & 0 & -0,03292 & 0,03292 & -0,1481 \\
 0 & 0 & 0 & 0 & 0,1481 & -0,1481 & 0,6667
 \end{bmatrix}$$

Agregacja wektora reakcji przyrzutowych od obciążenia parabolicznego

$$\underline{R}_{01} = \begin{bmatrix} -18 \\ -12 \\ -18 \\ 12 \end{bmatrix} \quad \underline{R}_{02} = \begin{bmatrix} 18,56 \\ 17,72 \\ 8,438 \end{bmatrix} \quad \underline{R}_{03} = \begin{bmatrix} -15,19 \\ -25,31 \\ 22,78 \end{bmatrix}$$

$$\underline{R}_0 = \begin{bmatrix} -18 \\ -12 \\ -18 + 18,56 \\ 12 + 17,72 \\ 8,438 - 15,19 \\ -25,31 \\ 22,78 \end{bmatrix} = \begin{bmatrix} -18 \\ -12 \\ 0,56 \\ 29,72 \\ -6,752 \\ -25,31 \\ 22,78 \end{bmatrix}$$

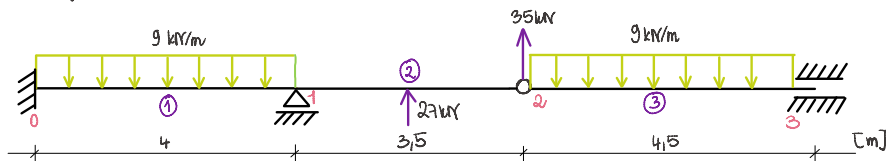
## Uwzględnienie warunków brzegowych

$$q_1=0, q_2=0, q_3=0, q_6=0, q_7=0$$

$$K = EI \begin{bmatrix} 0,1375 & 0,3750 & -0,1375 & 0,3750 & 0 & 0 & 0 \\ 0,3750 & 1 & -0,3750 & 0,5 & 0 & 0 & 0 \\ -0,1375 & 0,3750 & 0,1375 & -0,3750 & 0,06991 & 0 & 0 \\ 0,3750 & 0,5 & -0,1375 & 1,857 & -0,2449 & 0 & 0 \\ 0 & 0 & -0,03997 & -0,2449 & 0,1029 & -0,02892 & 0,1181 \\ 0 & 0 & 0 & 0 & -0,02892 & 0,02892 & -0,1181 \\ 0 & 0 & 0 & 0 & 0,1181 & -0,1181 & 0,6667 \end{bmatrix} \quad R_0 = \begin{bmatrix} -18 \\ -12 \\ -0,56 \\ 29,72 \\ -6,752 \\ -25,21 \\ 22,78 \end{bmatrix}$$

$$K_{red} = \begin{bmatrix} 1,857 & -0,2449 \\ -0,2449 & 0,1029 \end{bmatrix} \begin{matrix} 4 \\ 5 \end{matrix} \quad R_{red} = \begin{bmatrix} 29,72 \\ -6,752 \end{bmatrix} \begin{matrix} 4 \\ 5 \end{matrix}$$

## Wyznaczenie sektora obciążenia rozciąganych



$$P_{red} = \begin{bmatrix} 0 \\ -35 \end{bmatrix} \begin{matrix} 4 \\ 5 \end{matrix}$$

## Różnicanie równań

$$K_{red} q_{red} = P_{red} - R_{red}$$

$$EI \begin{bmatrix} 1,857 & -0,2449 \\ -0,2449 & 0,1029 \end{bmatrix} \begin{bmatrix} q_4 \\ q_5 \end{bmatrix} = \begin{bmatrix} 0 \\ -35 \end{bmatrix} - \begin{bmatrix} 29,72 \\ -6,752 \end{bmatrix}$$

$$EI \begin{bmatrix} 1,857 & -0,2449 \\ -0,2449 & 0,1029 \end{bmatrix} \begin{bmatrix} q_4 \\ q_5 \end{bmatrix} = \begin{bmatrix} -29,72 \\ -28,25 \end{bmatrix}$$

$$\begin{cases} 1,857EIq_4 - 0,2449EIq_5 = -29,72 \\ -0,2449EIq_4 + 0,1029EIq_5 = -28,25 \end{cases}$$

$$\begin{cases} q_4 = -\frac{7609}{EI} = -0,1844^\circ \\ q_5 = -\frac{455,64}{EI} = -0,01927 \text{ m} \end{cases}$$

## Nektory przemieszczeń dla elementów

$$\underline{q}_1' = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \end{bmatrix} = \frac{1}{EI} \begin{bmatrix} 0 \\ 0 \\ 0 \\ -76,09 \end{bmatrix}$$

$$\underline{q}_2' = \begin{bmatrix} q_5 \\ q_4 \\ q_6 \end{bmatrix} = \frac{1}{EI} \begin{bmatrix} 0 \\ -76,09 \\ -455,64 \end{bmatrix}$$

$$\underline{q}_3' = \begin{bmatrix} q_7 \\ q_6 \\ q_7 \end{bmatrix} = \frac{1}{EI} \begin{bmatrix} -455,64 \\ 0 \\ 0 \end{bmatrix}$$

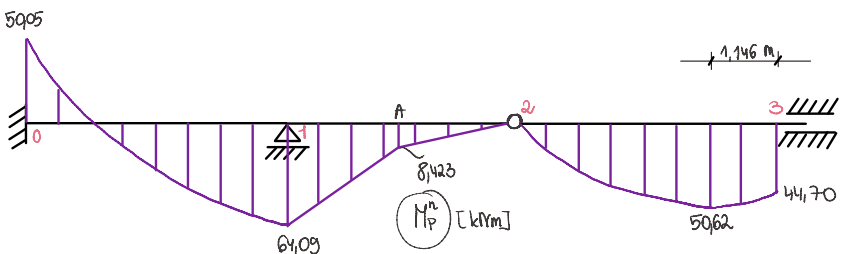
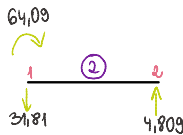
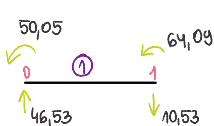
## Nektory reakcji węzłowych

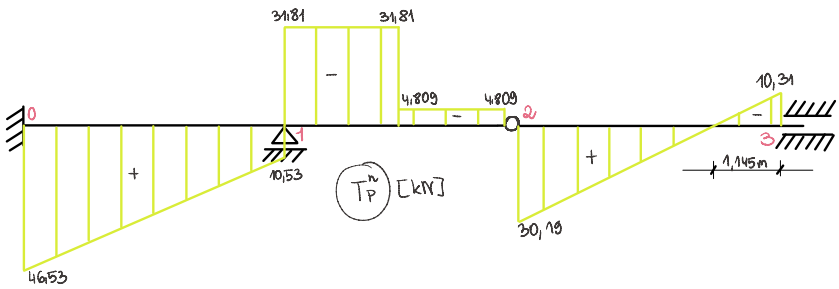
$$\underline{R}_1 = \underline{K}_1 \underline{q}_1' + \underline{R}_{01} = \underline{E} \cdot \begin{bmatrix} 0,1875 & 0,3750 & -0,1875 & 0,3750 \\ 0,3750 & 1 & -0,3750 & 0,5 \\ -0,1875 & -0,3750 & 0,1875 & -0,3750 \\ 0,3750 & 0,5 & -0,3750 & 1 \end{bmatrix} \cdot \frac{1}{EI} \begin{bmatrix} 0 \\ 0 \\ 0 \\ -76,09 \end{bmatrix} + \begin{bmatrix} -18 \\ -12 \\ -18 \\ 12 \end{bmatrix} = \begin{bmatrix} -46,53 \\ -50,05 \\ 10,53 \\ -64,09 \end{bmatrix}$$

$$\underline{R}_2 = \underline{K}_2 \underline{q}_2' + \underline{R}_{02} = \underline{E} \cdot \begin{bmatrix} 0,06997 & 0,2449 & -0,06997 \\ 0,2449 & 0,8571 & -0,2449 \\ -0,06997 & -0,2449 & 0,06997 \end{bmatrix} \cdot \frac{1}{EI} \begin{bmatrix} 0 \\ -76,09 \\ -455,64 \end{bmatrix} + \begin{bmatrix} 18,56 \\ 17,72 \\ 8,438 \end{bmatrix} = \begin{bmatrix} 31,81 \\ 64,09 \\ -4,809 \end{bmatrix}$$

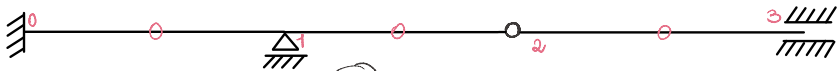
$$\underline{R}_3 = \underline{K}_3 \underline{q}_3' + \underline{R}_{03} = \underline{E} \cdot \begin{bmatrix} 0,03292 & -0,03292 & 0,1481 \\ -0,03292 & 0,03292 & -0,1481 \\ 0,1481 & -0,1481 & 0,6667 \end{bmatrix} \cdot \frac{1}{EI} \begin{bmatrix} -455,64 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} -15,19 \\ -25,31 \\ 22,38 \end{bmatrix} = \begin{bmatrix} -30,19 \\ -10,31 \\ -44,70 \end{bmatrix}$$

## Sily węzłowe





$T_P$  [kN]



$N_P$  [kN]

$$T(x) = -9 \cdot x + 10,53 = 0$$

$$x = 1,146 \text{ m}$$

$$\sum M^{(1/2)} = M_{\text{Ext}} + 9 \cdot 1,146 \cdot \frac{1,146}{2} - 44,70 - 10,32 \cdot 1,146 = 0$$

$$M_{\text{Ext}} = 50,62 \text{ kNm}$$

$$\sum M^{(1)} = 64,09 - 31,81 \cdot \frac{3,5}{2} + M_A = 0$$

$$M_A = -8,423 \text{ kNm}$$